# **Detecting UAVs Using Acoustic Camera**

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Abstract— Over the past decade, a huge increase in production and operation of Unmanned Aerial Vehicles (UAVs) has been present on a global scale. To maintain the required level of safety and to accommodate the expanding traffic, the governments worldwide have implemented regulations to operations of UAVs. Nonetheless, in recent years there have been numerous safety and security incidents with UAVs, which prompted an increase in research of surveillance and interdiction methods tailored for UAVs. Detection of UAVs using acoustic camera, which is the primary topic of this paper, is possible due to UAV's propeller noise which is predominant noise source, at least in multicopter UAVs. We performed a detectability test of a commonly used custom made UAV type multirotor with 6 motors. We concluded that small multirotor UAVs can be detected with acoustic camera, a human interpreter is necessary for detection due to the background noise, maximum detection range can be greater than with visual detection, and UAV detectability depends on UAV noise spectrum, its ratio to background noise, the dynamic range of acoustic camera, and its frequency resolution.

Keywords-UAV; acoustic camera; surveillance; detection.

## I. INTRODUCTION

Over the past decade, a huge increase in production and operation of UAVs has been present on a global scale. According to Federal Aviation Administration (FAA) Aerospace Forecast for fiscal years 2017-2037, there are currently over 1.1 million registered UAVs in the United States (US). By the year 2021, in the US alone, the number of registered UAVs is expected to reach 6 million units. Of these, three quarters will be hobbyist UAVs and model aircraft in the 0.25 kg – 25 kg category [1].

To maintain the required level of safety and to accommodate the expanding traffic, the governments worldwide have implemented regulations to operations of UAVs. In 2012, US government regulated operation of UAVs by publishing *Public Law 112-95 - FAA Modernization and Reform Act of 2012* [2]. Operation of UAVs in Europe has been regulated by the act of European Comission in 2008 with *Regulation (EC) No 216/2008* for UAVs heavier than 150 kilograms, and with national regulations for UAVs lighter than 150 kg [3]. In 2017,

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however, a new regulation was proposed with the purpose of regulating all categories of UAVs in European Union (EU) and it is expected to be adopted during the 2018 [4].

Notwithstanding the attempts at regulating the UAV operations, the increase in number of operations alone has increased the probability of incidents. In [5], UAV sighting reports published by FAA dating from December 17, 2013 to September 12, 2015 were analyzed. FAA reports were organized in two categories: Sightings, which included incidents where a pilot or an air traffic controller spotted an UAV flying within or near the flight paths of manned aircraft though not posing an immediate threat or collision, and Close Encounters, where a manned aircraft came close enough to an UAV that it met the FAA's definition of a "near mid-air collision" or close enough that there was a possible danger [5]. They have analyzed 921 incident reports and deduced that 35.5 % of recorded incidents were Close Encounters and that over 90 % of all incidents occurred above allowed maximum altitude [5].

For safety and security reasons, it is necessary to develop methods for detection and monitoring of UAV operations in predetermined areas. Conventional methods of UAV detection are using radars, visual detection, and thermal or acoustic sensors. Radar detection of UAVs based on differentiating Doppler signatures of various UAVs was successfully performed and described in [6] and [7]. However, there are obvious difficulties in using this method in urban areas. Visual detection method by analyzing images from cameras with image processing algorithms was proven somewhat successful, with shortcomings typical of visual identification systems, namely false positives in case of other flying objects (e.g., birds) [8].

Another method of UAV detection is thermal imaging, which can be used for ground-based detection or for airborne collision avoidance during night-time operations. To prove that UAV detection using thermal imaging can be used as a viable detection system, thermal images obtained via *FLIR Lepton* micro thermal camera mounted on a Raspberry Pi processing unit were analyzed [9]. UAVs used for testing were *DJI Phantom 4, Parrot AR.drone 2*, and one custom made hexacopter.

Beside conventional methods of detection, possibility of detecting UAVs controlled via wireless devices (such as *Parrot AR Drone*) was successfully tested [10]. Authors have successfully detected and gained control of targeted drone as third party users. One shortcoming of this detection method is requirement for a wireless receiver installed on UAV.

Detection using acoustic sensors relies on sound emission of different units. Authors in [11] state that UAV detection with acoustic array, unlike radar detection and visual detection methods, does not depend on the size of observed object for detection, but rather on the sound of the engine. For their method, however, a requirement is a comprehensive database of UAV sounds.

Detection of UAVs using acoustic camera, which is the primary topic of this paper, is possible due to their propeller noise, the predominant noise source, at least in multicopter UAVs. Propeller noise is composed of tonal and broadband components. Tonal component contains basic frequency and harmonics. The basic frequency  $f_1$  or Blade Pass Frequency (BPF) is the product of propeller rotation speed and number of propeller blades [12]:

$$BPF = N_{\rm R} N_{\rm B} \, 60^{-1},\tag{1}$$

where is:

*BPF* - basic frequency of tonal propeller component,  $N_{\rm R}$  - propeller rotation speed (rotations per minute),  $N_{\rm B}$  - number of propeller blades.

Besides the base frequency harmonic components also appear [12]:

$$f_{\rm N} = f_1 N, \tag{2}$$

where is:

 $f_{\rm N}$  - frequency of the n-th harmonic,

 $f_1$  - basic tonal frequency,

*N* - number of particular harmonic.

Besides propeller noise, UAV's noise consists of airframe and structure borne noise. Airframe noise is the result of air flow (wind around airframe). It is of the broadband flow mixing type, except where a resonant cavity is formed. Its main characteristic is a great dependence on UAV's speed. In multirotors, this type of noise is quite low. Structure borne noise results from airframe vibrations. Various vibration modes excite structural modes. Acoustic space again has its acoustic modes that are excited by structural modes. This noise is quite complex and in UAV operations it does not have a great importance.

The primary scope of this paper is detection possibility of UAVs using acoustic camera. In Section 2 of the paper, we describe the methods and apparatus used for the test. In Section 3, we show and interpret results of the test, and in the Section 4, we draw conclusions and suggest ideas for the future work.

# II. METHOD AND APPARATUS

## A. Test track

In order to test the ability of acoustic camera to detect small airborne UAV, we flew custom built UAV over a 170 m long test track (Figure 1). The goal was to determine at what distance the UAV could be detected without trying to identify it. UAV was flown at the approximately 15 m – 45 m above ground level and at a steady velocity of around 2 m/s. The test was performed on a relatively cold winter day (4 °C) with little to no wind. The terrain of the polygon was grassy, without significant noise sources and without any sound sources with predominant tonal components. The test was performed in the early afternoon. Equivalent A-weighted residual (background) noise was 42.5 dB with 41.3 dB exceeded for 99 % of the measured time.



Figure 1. Test track

## B. Acoustic sensor

For this test, the acoustic camera produced by The Faculty of Mechanical Engineering from Ljubljana, called SoundEye, has been used. SoundEye consists of a microphone array and an optical camera in the center. It can work in two different configurations, basic (Figure 2, left), with 30 microphones equally distributed on the circular disc carrier, and extended, with 54 microphones – 3 flat extensions with 8 microphones each attached to the basic circular carrier at the angle of 120° to each other (Figure 2, right). The camera has fixed Field-of-View (FOV) angles, horizontal FOV of 58° and vertical FOV of 44° (these are angles at which the scene is covered by both optical and acoustic camera). Detailed camera specifications can be found in Table 1.

The working principle of an acoustic camera is based on the microphone array's properties to form a highly directional beam. The signals from the microphones are acquired simultaneously or with known relative time delays to be able to use the phase difference between the signals. As the sound propagates in the air at a finite known speed, a sound source is perceived by the microphones at different time instants and at different sound intensities that depend on both the sound source location and the microphone location.

Specification	Description
Function	Imaging device used to locate
	and characterize sound sources
Producer	Faculty of mechanical
	engineering, Ljubljana, Slovenia
Configuration	Basic and extended
Number of microphones	30 (basic), 54 (extended)
Microphone frequency range	20 Hz – 20 kHz
Mapping frequency range	800 Hz – 12.5 kHz (basic),
	100 Hz - 12.5 kHz (extended)
Sampling frequency of AD	48 kHz
converter	
Sampling resolution	16 bit/sample
Algorithm	Cross Spectral Matrix
	Beamforming
Analysing spectrum	1/1 octave, 1/3 octave, FFT
Optical/acoustic covering angle	$\pm$ 58° horizontal, $\pm$ 44° vertical
Optical camera frame rate	30 fps
Operating distance	>5 m
Mains supply	USB
Disc diameter	0.4 m
Extension length	1 m
Weight	10 kg

One of the methods to obtain an acoustic image from the measurement of the microphone array is to use beamforming. By delaying each microphone signal relatively to each other and adding them together, the signals coming from a specific direction are amplified while signals coming from other directions are canceled. The power of this resulting signal is then calculated and reported on a power map at a pixel corresponding to the specific direction. The process is iterated for each direction where the power needs

TABLE I. SOUNDEYE ACOUSTIC CAMERA SPECIFICATIONS

to be computed. The algorithm to obtain acoustic picture used by SoundEye acoustic camera is Cross Spectral Matrix Beamforming. The working principle is presented graphically in Figure 3.



Figure 3. Two configurations of acoustic camera

The dynamic range of acoustic image (the ratio of the largest to the smallest intensity of sound that can be presented, measured in decibels) depends on the frequency of the sound source. For the frequencies above the 1000 Hz, dynamic range is 24 dB, while for the lowest frequencies is smaller – at the frequency of 100 Hz it is about 2 dB. This understanding is crucial for interpretation of acoustic images.

Figure 4 - Figure 6 present examples to better understand the interpretation of acoustic images. Directivity function of acoustic camera for a certain angle depending on the frequency is presented in Figure 4. For this theoretical example extended configuration of camera was used and the source that emits white noise (random signal having equal intensity at different frequencies, giving it a constant power



Figure 2. Working principle of the acoustic camera

spectral density) is situated right in the middle of the camera's FOV at the distance of 100 m (far field). Figure 4 shows the ability to distinguish the emitted sound levels of a single source at a selected frequency. The range of angles on the vertical axis is chosen to correspond to the horizontal FOV of acoustic camera and is equal to 58°. The angle of 90° is situated at the middle of the axis. Based on the calculation, the camera would show the acoustic image of the same size at a given frequency as presented in Figure 4. For example, at the frequency of 1000 Hz the red area (highest level) will be slightly larger than the red area at a frequency of 10000 Hz, although the noise emission at both frequencies is the same. The ratio between dark red and dark blue color is 24 dB. At the frequency range between 1000 Hz and 12500 Hz, the dynamic range of the acoustic image is 24 dB. This does not apply to a frequency range below 1000 Hz.



Figure 4. Directivity function of acoustic camera in the frequency range 1000 Hz - 12000 Hz with acoustic image dynamic range of 24 dB

Figure 5 shows directivity function of acoustic camera in the frequency range 100 Hz - 1000 Hz with acoustic image dynamic range of 5 dB.



Figure 5. Directivity function of acoustic camera in the frequency range 100 Hz - 1000 Hz with acoustic image dynamic range of 5 dB

As can be seen, dynamic range is much narrower than that in Figure 4, especially at frequencies lower than 200 Hz (for the same sound emission at all frequencies). If the source would emit a sound at 100 Hz (source location right in the middle of the camera's FOV and at the distance of 100 m) and if the camera would have image dynamics (scale on the right side of the characteristics) 5 dB, the algorithm would calculate the acoustic image, which would be shown in red over the entire picture.

If the dynamic range would be reduced to 0.5 dB, the algorithm would calculate the acoustic image with characteristics as shown in Figure 6. A large red circle would be displayed in more than half of the image.



Figure 6. Directivity function of acoustic camera in the frequency range 100 Hz - 1000 Hz with acoustic image dynamic range of 0.5 dB

The results of the calculation of the acoustic image by an acoustic camera algorithm at frequencies lower than 1000 Hz and especially lower than 500 Hz should be considered only conditionally, both in terms of the range of noise level and in terms of the exact position of the noise source. At these frequencies, the dynamic range of acoustic images, some of which are presented in the results at the next paragraph, is set to lower values - from 0.1 dB to 2 dB.

# C. UAV

A custom built hexacopter was used in this test. The specifications are available in Table 2.

Parameter	Description
Size (w/o propellers)	$75 \times 75 \times 37$ cm
Weight	4420 g
Number of motors	6
Motor power	480 W
Motor type	Outrunner
Battery	LiPo, 6S, 5000 mAh
Propeller type	2-blade
Propeller size	12"

# TABLE II. SPECIFICATIONS OF THE HEXACOPTER USED IN TESTING

The most important parameter which determines UAVs acoustic footprint is propeller rotation speed. This UAV has 6 motors and their rotation speed varies within certain limits to achieve a satisfactory control and stability of the UAV. This rotation speed range is unknown so we did 1/3 octave band premeasurements of its noise to define a frequency band where basic frequency of tonal propeller component and its harmonics are situated.

# III. RESULTS AND DISCUSSION

First, we did 1/3 octave band measurements of UAV's noise to define a predominant frequency bands. The noise was measured by means of Nor140 Sound Analyzer with an extensive set of functions available in its expanded version. UAV's noise was recorded in time period of 5 s at the distance of 20 m at stabilized UAV flight mode. The noise levels were calculated and the characteristics are presented in Figure 7.



Figure 7. One-third octave band measurement results of UAVs noise

Residual noise is presented in blue color and the UAV's noise in green color. It is obvious that the UAV has broadband noise with basic frequency of tonal propeller component in 1/3 octave bands of central frequency of 125 Hz or 160 Hz. The difference of UAVs noise and background noise is at least 20 dB for the frequency range 100 Hz – 20 kHz.

Next four figures present the most interesting results of UAV visibility measurements using acoustic camera. All figures consist of four parts. At the top left side is situated a black and white photograph with the indicated position of the UAV. At the top right side is the overall spectrogram with the indicated part of the spectrogram (frequency components which originate from the UAV) used for calculation of specific acoustic image.

At the bottom left side is the acoustic image calculated from overall spectrogram and at the bottom right side is the acoustic image calculated from indicated part of the spectrogram. Measurement results at the distance of the 20 m are presented in Figure 8.



Figure 8. Measurement results at the distance of 20 m

UAV is visually clearly visible. It stands out as the dominant noise source within the overall sound image. The overall spectrogram highly expresses frequency components that come from the UAV. By using the selected part of the spectrogram, after signal processing, it is possible to determine the location of the UAV very well.



Figure 9. Measurement results at the distance of 60 m

Results of the measurements at the distance of 60 m are presented in Figure 9. UAV is discernible visually. It stands out as the dominant noise source within the overall sound image. The spectrogram shows frequency components that come from the UAV. By using the selected part of the spectrogram, after signal processing, it is possible to determine the location of the UAV.

Measurement results at the distance of the 100 m are presented in Figure 10. The UAV is visually noticeable. Within the overall sound image it does not stands out. In the spectrogram, the frequency components that come from the UAV are poorly visualized. By using the selected part of the spectrogram, after signal processing, it is possible to determine the location of the UAV.



Figure 10. Measurement results at the distance of 100 m

Measurement results at the distance of the 170 m are presented at Figure 11.



Figure 11. Measurement results at the distance of 170 m

The UAV is visually hardly noticeable. Within the overall acoustic image, it does not stand out. In the spectrogram, the frequency components that originate from the UAV are poorly visualized. By using the selected part of the spectrogram, after signal processing, it is possible to determine the location of the UAV with uncertainty. This is the detection limit based on the existing background noise.

# IV. CONCLUSIONS

We have performed a detectability test of commonly used custom-made type UAVs. Our goal was to determine whether an acoustic sensor could be used to detect multirotor UAVs for the purpose of air traffic surveillance or collision avoidance. To achieve this, we have flown a custom-built UAV over a test track and recorded its movement with the SoundEye acoustic camera.

We concluded that:

• Small multirotor UAVs can be detected with acoustic camera in some conditions;

- Basic four parameters on which detectability depends on are: UAV noise spectrum, its ratio to background noise, the dynamic range of acoustic camera, and its frequency resolution;
- Due to background noise, human interpreter is necessary in the detection process;
- Maximum range of detection can be greater than visual detection;
- Due to necessity of human interpreter and time for processing, it is questionable whether the acoustic camera can be used for air traffic surveillance purposes.

In the future work, we will test detectability of UAVs against noisier background conditions. A more rigorous test of detectability will be performed with UAVs appearing from unknown directions. Finally, we will test methods for reducing the noise signature of an UAV.

#### References

- [1] Federal Aviation Administration, "FAA Aerospace Forecast -Fiscal Years 2017-2037", United States Department of Transportation, Washington, 2017.
- [2] United States, "Public Law 112 95 FAA Modernization and Reform Act of 2012", U.S. Goverment Publishing Office, Washington, 2012.
- [3] European Comission, "Regulation (EC) No 216/2008", Official Journal of the European Union, Brussels, 2008.
- [4] European Aviation Safety Agency, "Notice of Proposed Amendment 2017-05 (A), Introduction of a regulatory framework for the operation of drones, Unmanned aircraft system operations in the open and specific category", EASA, 2017.
- [5] D. Gettinger and M.A. Holland, "Drone Sightings and Close Encounters: An Analysis", Center for the Study of the Drone at Bard College, New York. 2015.
- [6] F. Hoffmann, M. Ritchie, F. Fioranelli, A. Charlish, and H. Griffiths, "Micro-Doppler Based Detection and Tracking of UAVs with Multistatic Radar", in IEEE Radar Conference, Philadelphia. 2016, pp. 1-6
- [7] A. Moses, M. J. Rutherford, and K. P. Valvanis, "Radar-Based Detection and Identification for Miniature Air Vehicles", in 2011 IEEE Multi-Conference on Systems and Control, Denver, 2011, pp. 933-940
- [8] T. Zsedrovits et al., "Collision avoidance for UAV using visual detection", in 2011 IEEE International Symposium of Circuits and Systems, Rio de Janeiro, 2011, pp. 2173-2176
- [9] P. Andraši, T. Radišić, M. Muštra, and J. Ivošević, "Nighttime Detection of UAVs using Thermal Infrared Camera", InAIR Conference 2017. Prague, 2017, pp. 183-190
- [10] M. Peacock and M. N. Johnstone, "Towards detection and control of civilian unmanned aerial vehicles", in 14th Australian Information Warfare Conference, Perth, 2013, pp. 9-15
- [11] E. E. Case, A. M. Zelnio, and B.D. Rigling, "Low-Cost Acoustic Array for Small UAV Detection and Tracking", in Aerospace and Electronics Conference, Dayton, 2008, pp. 110-113
- [12] D. Miljković, J. Ivošević, and T. Bucak, "Two vs. three blade propeller - cockpit noise comparison", International Congress Alps Adria Acoustics Association 2012 Proceedings, Zadar, Croatia, 2012, pp. 1-5